

AD-A080049

TECHNICAL  
LIBRARY

AD A080049

# STUDY OF THE MELTING BEHAVIOR OF YAG SINGLE CRYSTAL BY OPTICAL DIFFERENTIAL THERMAL ANALYSIS

JAROSLAV L. CASLAVSKY and DENNIS J. VIECHNICKI  
CERAMICS RESEARCH DIVISION

November 1979

Approved for public release; distribution unlimited.

ARMY MATERIALS AND MECHANICS RESEARCH CENTER  
Watertown, Massachusetts 02172

The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

Mention of any trade names or manufacturers in this report shall not be construed as advertising nor as an official indorsement or approval of such products or companies by the United States Government.

#### DISPOSITION INSTRUCTIONS

Destroy this report when it is no longer needed.  
Do not return it to the originator.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AMMRC TR 79-56	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) STUDY OF THE MELTING BEHAVIOR OF YAG SINGLE CRYSTAL BY OPTICAL DIFFERENTIAL THERMAL ANALYSIS		5. TYPE OF REPORT & PERIOD COVERED Final Report
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Jaroslav L. Caslavsky and Dennis J. Viechnicki		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Army Materials and Mechanics Research Center Watertown, Massachusetts 02172 DRXMR-EO		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS D/A Project: 1T162105AH84 AMCMS Code: 612105 Agency Accession: DA 101
11. CONTROLLING OFFICE NAME AND ADDRESS U. S. Army Materiel Development and Readiness Command, Alexandria, Virginia 22333		12. REPORT DATE November 1979
		13. NUMBER OF PAGES 17
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Yttrium aluminum garnet (YAG) Phase equilibria Laser materials Optical differential thermal analysis (ODTA)		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  (SEE REVERSE SIDE)		

DD

FORM  
1 JAN 73

1473

EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

Block No. 20

## ABSTRACT

The melting point of yttrium aluminum garnet (YAG), reinvestigated by optical differential thermal analysis (ODTA), was found to be  $1940 \pm 7$  C. Above this temperature YAG liquids are opaque, suggesting the presence of two immiscible liquids. In the composition range 10.0 to 47.5 mol. %  $Y_2O_3$ ; crystallization of the equilibrium phases can only occur in the presence of YAG nuclei; otherwise solidification of  $YAlO_3$  and  $Al_2O_3$  will take place. A metastable phase diagram has been defined with a metastable eutectic at 23 mol. %  $Y_2O_3$  - 77 mol. %  $Al_2O_3$  and  $1702 \pm 7$  C.  $YAlO_3$  (perovskite) was found to melt incongruently with a peritectic temperature of  $1916 \pm 7$  C and a liquidus temperature of  $1934 \pm 7$  C.  $YAlO_3$  formed during metastable solidification transforms to YAG in the presence of  $Al_2O_3$  at  $1418 \pm 7$  C. It is suggested that the metastability arises from the difficulty of the aluminum to attain fourfold coordination in the YAG structure.

## CONTENTS

	Page
INTRODUCTION. . . . .	1
MEASUREMENTS OF THE YAG MELTING POINT . . . . .	1
OPTICAL DIFFERENTIAL THERMAL ANALYSIS (ODTA). . . . .	3
SENSITIVITY OF THE ODTA APPARATUS . . . . .	6
MELTING POINT OF YAG. . . . .	7
METASTABILITY	
Formation of Two Liquids . . . . .	9
Change of Aluminum Coordination. . . . .	11
CONCLUSIONS . . . . .	13
ACKNOWLEDGMENTS . . . . .	14

## INTRODUCTION

During the course of growing large (7.5 cm in diameter and 10 cm high) yttrium aluminum garnet (YAG) single crystals by vertical solidification (Heat Exchanger Method (HEM)),<sup>1</sup> two crucial factors were recognized as necessary to grow single crystals free of scattering centers:

(a) the starting material has to contain only the  $Y_3Al_5O_{12}$  phase;<sup>2</sup>

(b) the melting point of the garnet phase has to be known with the greatest possible accuracy in order to prevent melting of a seed crystal while simultaneously insuring complete melting of the charge.

Published melting points of YAG are given as 1930 C<sup>3,4</sup> and 1970 C.<sup>5-7</sup> By contrast, the temperature of thermoarrest observed during the melting of 2000-g batches of sintered YAG materials indicated that the melting point of YAG is neither 1930 C nor 1970 C, but rather lies between those temperatures. In view of the conflicting information on melting points of YAG it appeared that a new determination of melting point and a study of YAG melting behaviour would be of value.

## MEASUREMENTS OF THE YAG MELTING POINT

At the beginning of this investigation the melting point of YAG was measured by four commonly used experimental techniques: differential thermal analysis (DTA), hot wire microscopy, an iridium strip furnace, and direct observation of the sample melting through an optical pyrometer (DOSMTOP).

Differential thermal analysis was found unsuitable due to instability of the emf of W-3%Re versus W-25%Re thermocouple wires at temperatures over 1800 C. The melting points as determined by the hot wire microscope, strip furnace, and DOSMTOP are listed in Table 1. The average temperature 1968 C obtained by the hot wire microscope is in good agreement with the 1970 C melting point reported by Warshaw and Roy,<sup>5</sup> Olds and Otto,<sup>6</sup> and Abell et al.<sup>7</sup> On the other hand, the average melting points obtained by the other methods were too high, and a particularly large standard deviation of the DOSMTOP method measurements indicated a possible error in the concept of this method.

Despite the scatter in the YAG melting point measurements, the 2058 C melting point of  $Al_2O_3$  as determined by the DOSMTOP agreed well with the 2055 ±

1. VIECHNICKI, D. J., and SCHMID, F. *Crystal Growth Using the Heat Exchanger Method (HEM)*. J. Crystal Growth, v. 26, 1974, p. 162-164.
2. VIECHNICKI, D. J., and CASLAVSKY, J. L. *Solid State Formation of Nd:Y<sub>3</sub>Al<sub>5</sub>O<sub>12</sub> (Nd:YAG)*. Army Materials and Mechanics Research Center, AMMRC TR 78-7, February 1978.
3. TOROPOV, N. A., BONDAR, I. A., GALADHOV, F. Ya., NIKOGOSYAN, Kh. S., and VINOGRADOVA, N. V. *Izv. Akad. Nauk. SSSR, Ser. Khim.*, v. 7, 1969, p. 1158.
4. MIZUMO, M., and NOGUCHI, T. *Rep. Gov. Ind. Res. Inst. of Nagoya*, v. 16, 1967, p. 171.
5. WARSHAW, I., and ROY, R. *Stable and Metastable Equilibria in the Systems Y<sub>2</sub>O<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> and Gd<sub>2</sub>O<sub>3</sub>-Fe<sub>2</sub>O<sub>3</sub>*. J. Amer. Cer. Soc., v. 42, 1959, p. 434-438.
6. OLDS, L. E., and OTTO, H. E. *Phase Diagrams of Ceramists*. J. Amer. Cer. Soc., E. M. Levin, et al., ed., 1969, Figure 311.
7. ABELL, J. S., HARRIS, J. R., COCKAYNE, B., and LENT, B. *An Investigation of Phase Stability in the Y<sub>2</sub>O<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> System*. J. Mater. Sci., v. 9, 1974, p. 527-537.

Table 1. YAG MELTING POINTS MEASUREMENT

Sample	Hot Wire Microscope Deg C	Strip Furnace Deg C	DOSMTOP* Method Deg C
1	1969	1987	1990
2	1969	1992	1970
3	1971	1991	1965
4	1970	1988	1974
5	1970	1975	1974
6	1971	1986	1992
7	1965	1986	1960
8	1969	1991	1962
9	1968	1990	1988
10	1968	1992	1960
11	1967	1989	1992
12	1970	1988	1996
13	1971	1990	1965
14	1968	1990	1982
15	1968	1988	1982
16	1969	1990	1988
Average	1968.94	1988.31	1978.75
Standard Deviation		1.61	4.03
			13.32

\*Direct observation of sample melting through the optical pyrometer.

6 C melting point reported by Jones<sup>8</sup> and Schneider and McDaniel.<sup>9</sup> Since even better agreement was found between the tabulated melting point of platinum and those measured by DOSMTOP, it was inferred that the inconsistency in the measurements of the YAG melting point was due to some intrinsic property of YAG rather than to the method itself.

Since the literature survey and results obtained show that the YAG melting point lies in the temperature range between 1930 C and 1975 C, another indirect experimental method was used to better define the melting point of YAG. The method is based on Warshaw and Roy's<sup>5</sup> observation of the ease with which  $YAlO_3$  forms from a melt of  $Y_3Al_5O_{12}$  composition. The experimental arrangement was identical to that used in the DOSMTOP determination of YAG melting points with the difference that the YAG crystal was brought only to a desired temperature and cooled down. The sample was then examined by a petrographic microscope and powder X-ray diffraction analysis. Results of both examinations are presented in Table 2.

$YAlO_3$  was found in the sample of YAG crystal heated to 1930 C which implied that YAG started to melt at this temperature. Since the sample was held at this temperature for a short period of time, it was assumed that an insufficient amount of heat was supplied to the sample to achieve complete melting. To test this assumption, large samples of YAG crystals were heated as in the previous experiment except that the temperature was stabilized at a certain value measured with the optical pyrometer, which then was replaced with a camera, and the sample was

8. JONES, T. P. *The Melting Point of  $Al_2O_3$  in Vacuum*. J. Aust. Cer. Soc., v. 5, 1969, p. 41-44.

9. SCHNEIDER, S. J., and McDANIEL, C. L. *Effect of Environment Upon the Melting Point of  $Al_2O_3$* . J. Research of NBS, v. 71A, 1967, p. 317-333.



Table 2. MICROSCOPIC AND X-RAY EXAMINATION OF YAG SAMPLES  
ANNEALED AT DIFFERENT TEMPERATURES

Blackbody Enclosure Temperature, Deg C	Microscopic Observation	Phase Present
1900	N/C*	YAG
1905	N/C	YAG
1910	N/C	YAG
1915	N/C	YAG
1920	N/C	YAG
1925	N/C	YAG
1930	N/C	YAG + Trace of $\text{YAlO}_3$
1935	N/C	$\alpha\text{Al}_2\text{O}_3$ + $\text{YAlO}_3$ + Traces of YAG
1940	N/C	$\alpha\text{Al}_2\text{O}_3$ + $\text{YAlO}_3$
1945	Rounding of edges	$\alpha\text{Al}_2\text{O}_3$ + $\text{YAlO}_3$
1950	Edges more rounded	$\alpha\text{Al}_2\text{O}_3$ + $\text{YAlO}_3$
1955	Sample Collapsed	$\alpha\text{Al}_2\text{O}_3$ + $\text{YAlO}_3$

\*No change

photographed. This procedure was repeated for all the temperatures indicated in Figure 1 until collapse of the sample occurred. This experiment confirmed previous findings that YAG melts or begins to melt at 1930 C and simultaneously indicated that the length of time at temperature was not the only factor determining collapse of the sample. All experiments thus far showed that the collapse of the YAG single crystal was not a sensitive indicator of the melting. Hence, a method sensitive to the change of the latent heat of melting had to be used, but for reasons previously discussed it could not employ thermocouples.

During the course of this investigation it was noticed that before the YAG crystals collapsed they first brightened and then darkened considerably. These brightening and darkening phenomena were measured and recorded in Table 3 for several YAG samples. The 1928 C brightening temperature was close to the 1930 C melting point of YAG reported by Toropov et al.<sup>3</sup> and Mizumo and Noguchi,<sup>4</sup> while the 1935 C darkening temperature was near the 1937 C thermoarrest temperature observed during the melting of large boules of sintered YAG material in the crystal growth furnace; it was inferred that this optical effect was associated with the melting of YAG and also was a sensitive indicator of this melting.

#### OPTICAL DIFFERENTIAL THERMAL ANALYSIS (ODTA)

Since the brightening and darkening effects of YAG are easily perceivable with the eye, it became evident that a differential curve could be registered by an optical apparatus utilizing the following radiation principles. When radiant energy strikes a material surface, part of the radiation is absorbed



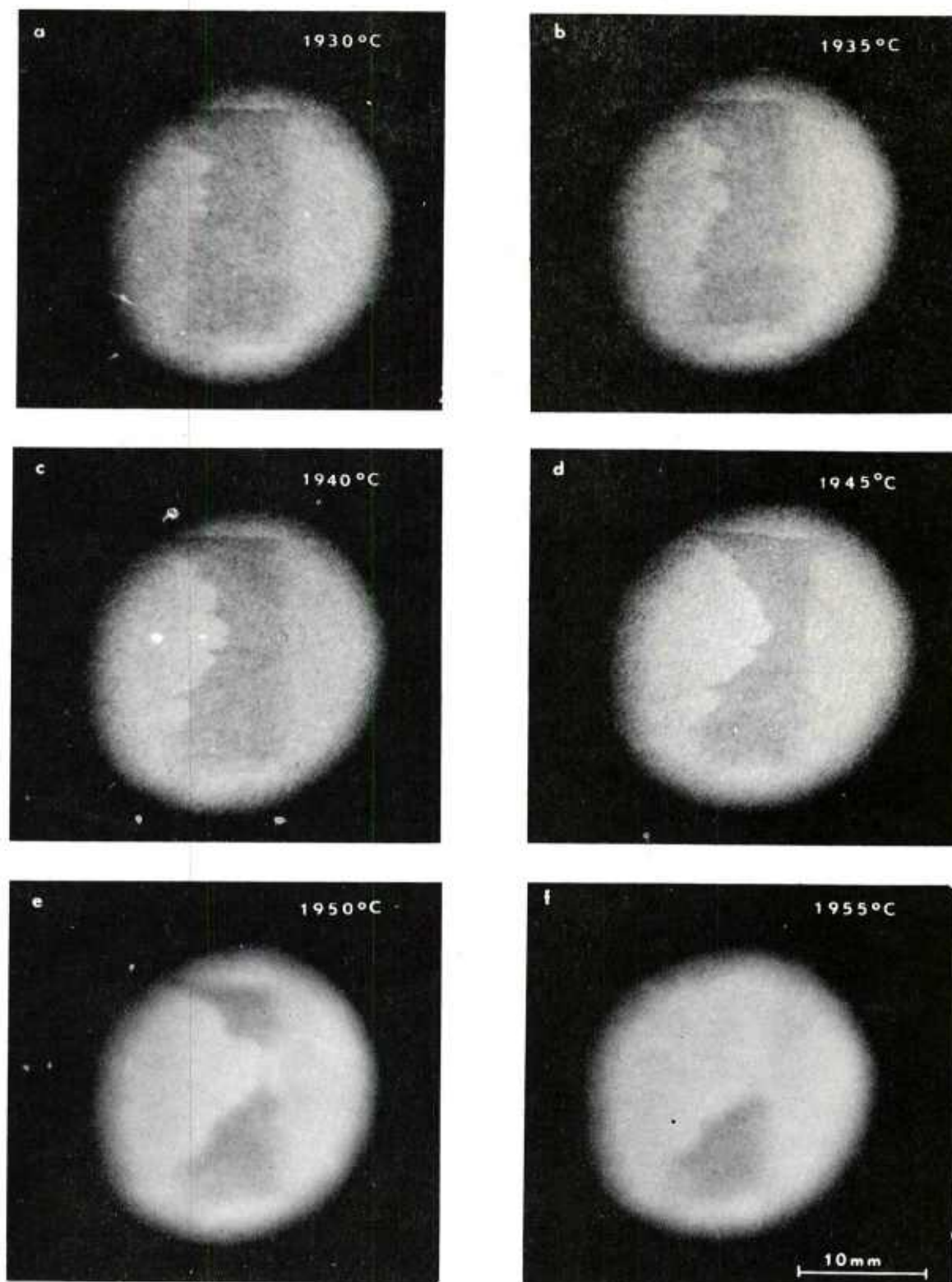


Figure 1. Photographs of the progress in melting of YAG single crystal as run with increasing temperature.

and part is reflected. A body which does not reflect any radiation is called a blackbody. On the other hand, at any given temperature a real object will radiate only a fraction as much energy as the blackbody and that fraction is called emissivity. Emissivity of an object varies widely with its temperature and its surface condition. In conformity with radiation principles the optical differential curve is obtained by differentiation of current signals from two infrared detectors. A block schematic is presented in Figure 2. Detector ① monitors the temperature of the blackbody containing the sample while the detector ② measures the brightness temperature of the sample. The heat capacity of the blackbody enclosure ⑤ is considerably higher than the heat capacity of the sample ⑥. Accordingly, the blackbody temperature is not affected by temperature changes taking place in the sample. Therefore, the real temperature of the sample is the temperature of the blackbody enclosure. First measurements obtained by this apparatus revealed a high degree of uncertainty and indeed a real problem of how to relate maxima and minima of the ODTA curve to the temperature scale. At this point, it was realized that the infrared detector generates a current proportional to the intensity of radiation, but that its intensity, as well as the signal current, is a highly nonlinear function of the temperature. The differentiation of these mutually nonlinear signals resulted in a curve with both endothermic and exothermic peaks, irregularly shaped, and often obscured by a drift of the zero line. Linearization ⑦ of the current signals with respect to the temperature prior to differentiation ⑧ made the differential curve legible while simultaneously eliminating the zero drift. The ODTA record of melting an  $\text{Al}_2\text{O}_3$  single crystal is shown in Figure 3. Using this apparatus melting points of 2051 C were observed for the Verneuil-grown  $\text{Al}_2\text{O}_3$  single crystal, 2053 C for the HEM-grown  $\text{Al}_2\text{O}_3$  crystal, and 2056 C for the National Bureau of Standards

Table 3. MEASUREMENT OF BRIGHTENING AND DARKENING TEMPERATURE OF YAG SINGLE CRYSTAL

Sample	Temperature, Deg C	
	Brightening	Darkening
1	1929	1934
2	1926	1930
3	1931	1936
4	1927	1931
5	1928	1934
6	1930	1936
7	1925	1932
8	1927	1932
9	1928	1936
10	1931	1937
11	1926	1934
12	1929	1938
13	1925	1937
14	1924	1936
15	1930	1935
<hr/>		
Average Temperature	1927.73	1934.53
Standard Deviation	2.25	2.39

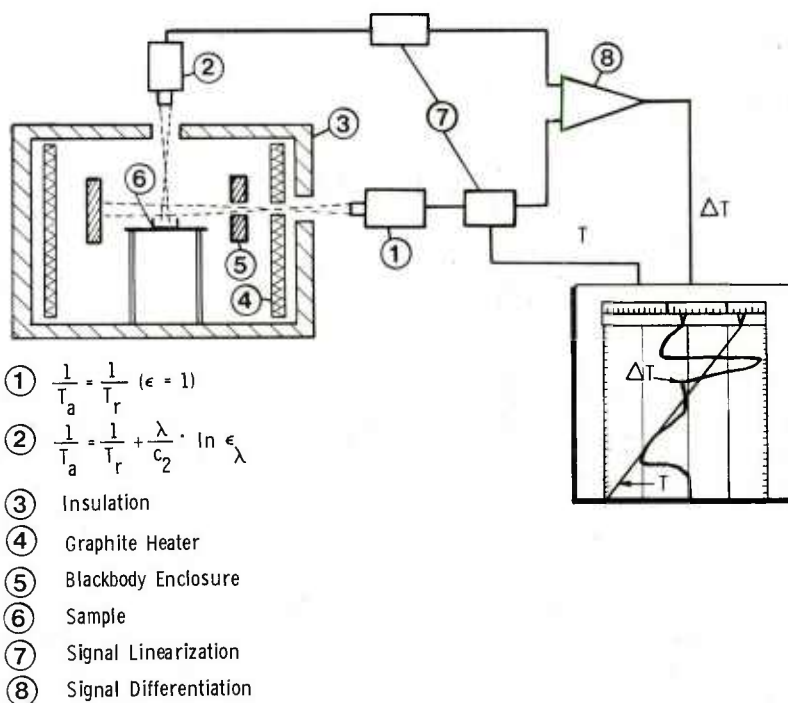


Figure 2. Schematic of optical differential thermal analysis apparatus.

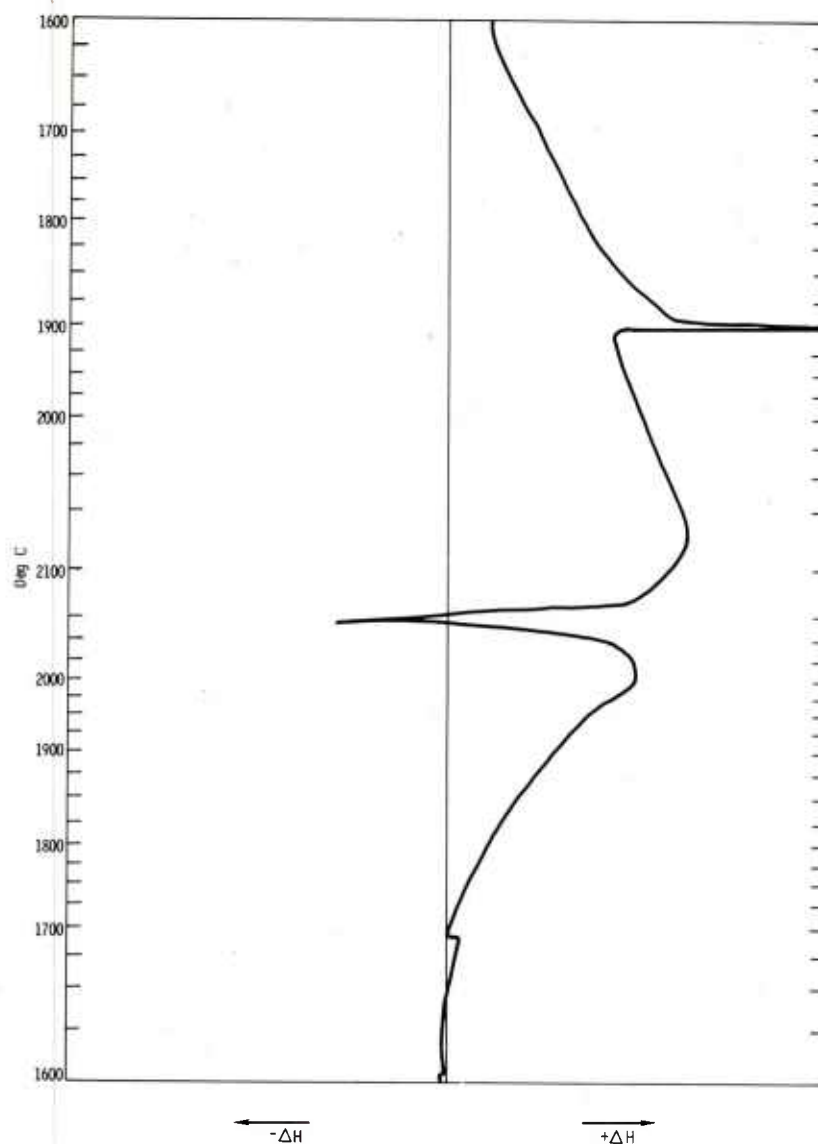


Figure 3. ODTA curve of melting and freezing of  $\alpha$   $\text{Al}_2\text{O}_3$ . (NBS standard reference material No. 742).

$\text{Al}_2\text{O}_3$  powder. These data show good agreement with the data reported by Jones<sup>8</sup> and Schneider and McDaniel,<sup>9</sup> and confirmed the suitability of the ODTA technique for determination of melting points at high temperatures.

### SENSITIVITY OF THE ODTA APPARATUS

In the final version of the ODTA apparatus, automatic optical pyrometers of the MODLINE 2000 series\* are used. The current signal is linearized with respect to the temperature with a  $\pm 10\%$  accuracy in the range between 1200 C and 2200 C. In this range the linearized output is 0 to +100 mV dc. The magnitude

\*Manufactured by IRCON Inc., Skokie, Illinois

of the differential signal was evaluated experimentally from an endothermic minimum formed when a YAG crystal was heated at the rate of 7 C/min. The minimum was 32 C deep and 30 C wide. For comparison of the ODTA and DTA data, the YAG crystal was melted under the same experimental conditions, but this time a differential curve was recorded by thermocouples. The DTA endothermic minimum was only 6 C deep and 64 C wide, and indicated an approximately 30 C higher melting temperature. The better resolution of optical measurements compared to thermocouple measurements is attributed to contactless sensing of temperature, which eliminates the reaction heat loss due to the heat capacity and conductivity of thermocouples. The reproducibility of melting points as determined by the ODTA is  $\pm 7$  C in the range between 1200 C and 2200 C.

### MELTING POINT OF YAG

The ODTA curve shown in Figure 4 depicts melting and freezing of a YAG single crystal. The first exothermic maximum at 1926 C falls in the range of the brightening of YAG which precedes its melting, as imaged by the endothermic minimum at 1939 C. With decreasing temperature, a sharp exothermic maximum at 1632 C indicates a spontaneous solidification which occurred at a high degree of supercooling. This 307 C supercooling suggests that under certain conditions the YAG melt may be able to adopt an alternative path of solidification, even though Abell et al.<sup>7</sup> considered YAG to be the only unambiguously stable phase in the

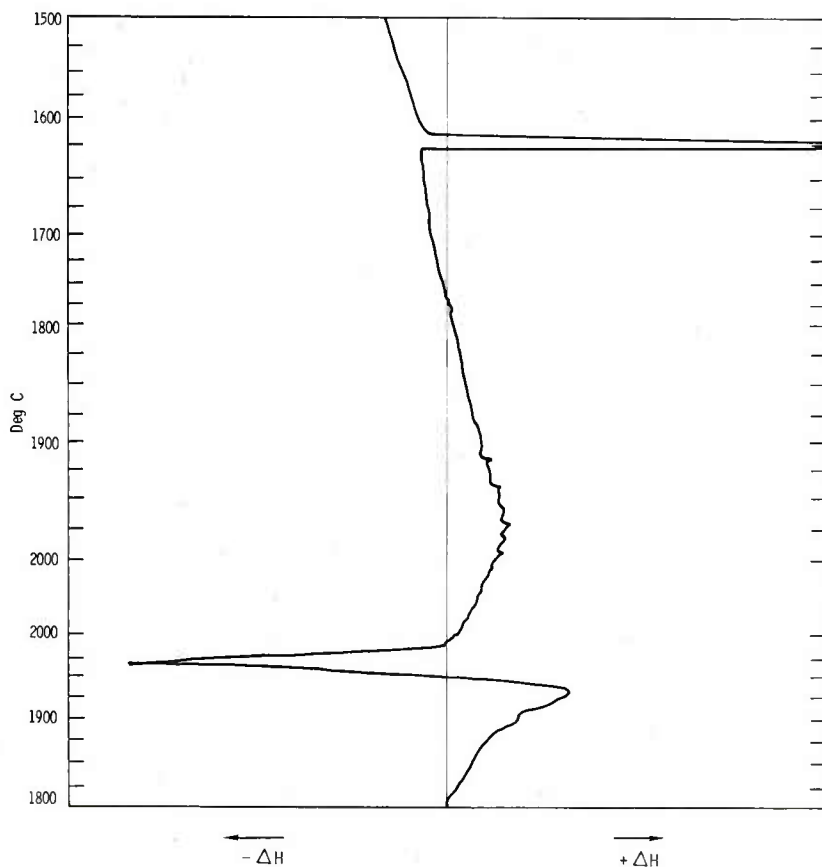


Figure 4. ODTA curve of melting and freezing of YAG single crystal.

$\text{Al}_2\text{O}_3$ - $\text{Y}_2\text{O}_3$  system. To investigate whether the high degree of supercooling is pertinent to the YAG melt solidification or to some other phenomena, the solidified material which remained in the crucible after ODTA of YAG was subjected to a second analysis, results of which are shown in Figure 5. Two endothermic maxima, the first at 1702 C and the second at 1855 C, substantiate the X-ray evidence which revealed that YAG, after being melted, solidifies into a mixture of  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$  in the absence of YAG nuclei. The minimum at  $1702 \pm 7$  C corresponds to the temperature of the metastable eutectic formed between  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$ , while the metastable liquidus temperature for the particular mixture is 1855 C. In an effort to define the metastable phase diagram between  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$ , mixtures of  $\text{Al}_2\text{O}_3$  and  $\text{Y}_2\text{O}_3$  were reacted at 1100 C for 48 hours and analyzed by ODTA. The melting of samples reacted in the solid state followed the equilibrium phase diagram shown by solid lines in Figure 6. By remelting solidified samples, the metastable diagram shown by dotted lines was defined. It should be noted that  $\text{YAlO}_3$  was found to melt incongruently with a peritectic temperature at  $1916 \pm 7$  C and a liquidus temperature at  $1934 \pm 7$  C. Supporting data are given in Table 4.

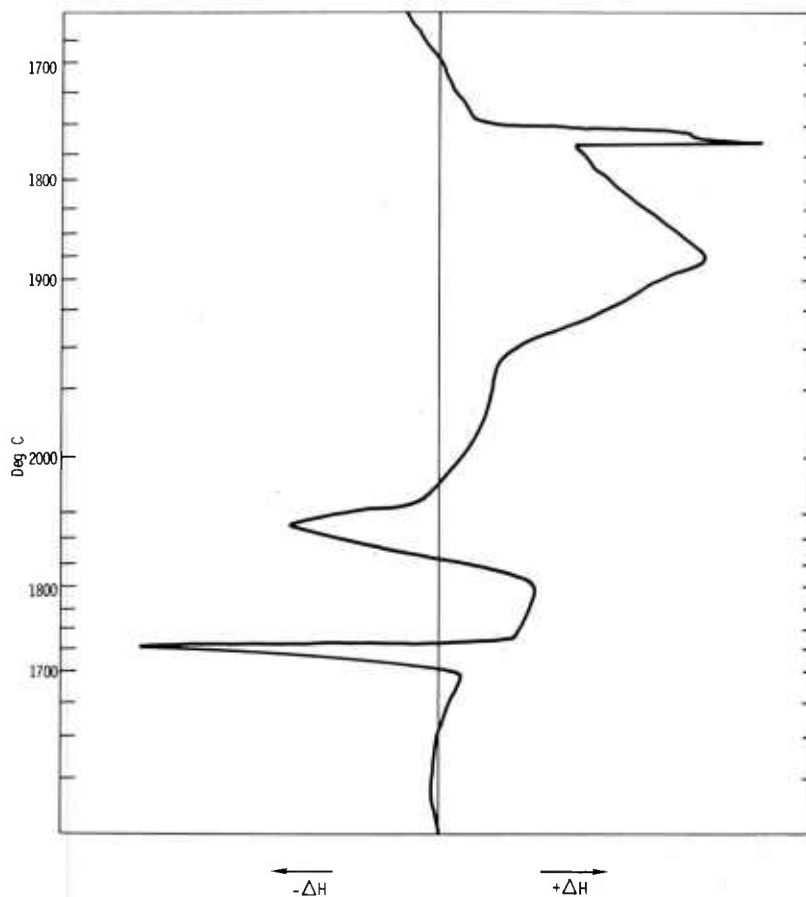


Figure 5. ODTA curve of melting and freezing of YAG melt heated up to 2000 C and subsequently cooled to 1600 C.



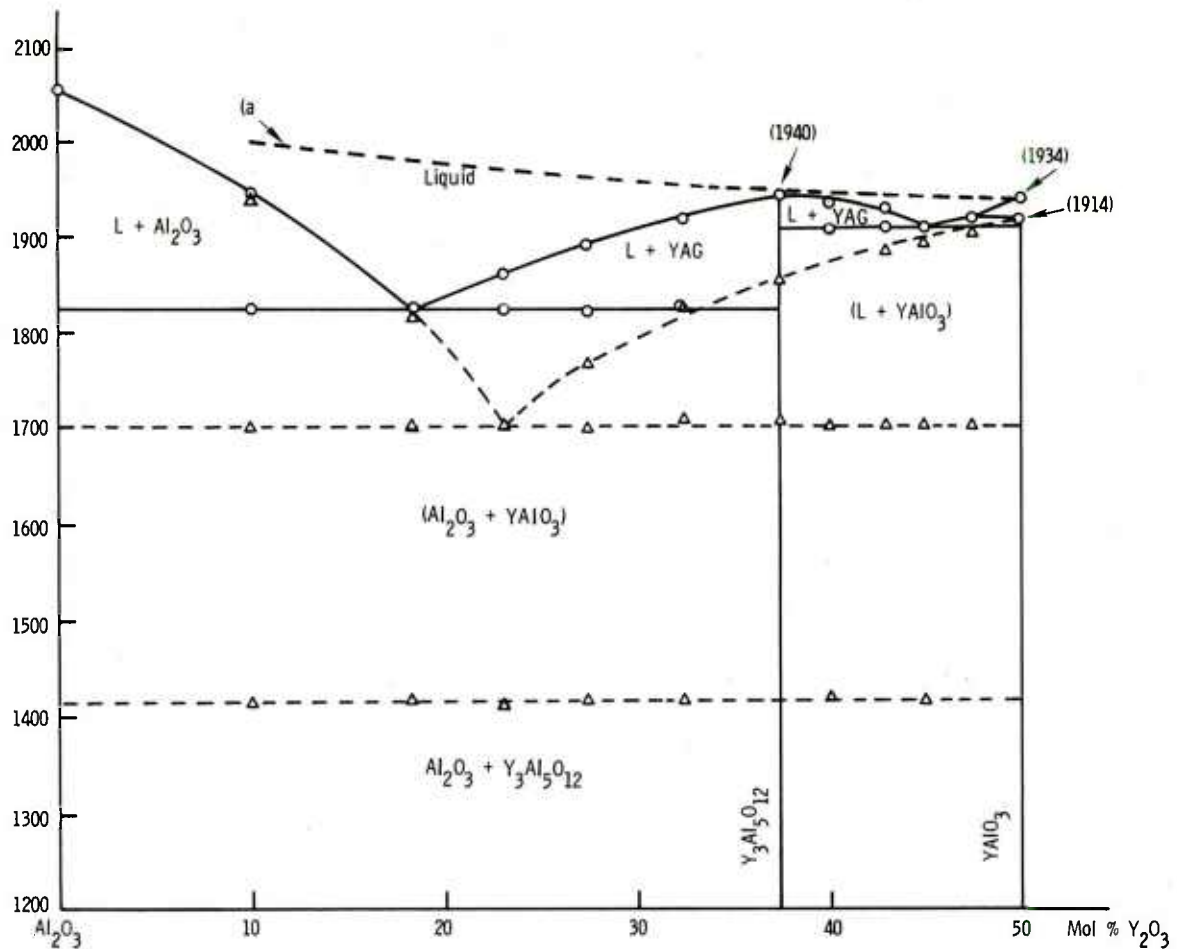


Figure 6. Phase diagram of the alumina-rich portion of the  $\text{Al}_2\text{O}_3\text{-Y}_2\text{O}_3$  system. Equilibrium phase diagram is shown in solid lines; pertinent phase fields are labeled without parentheses. The metastable phase diagram is superimposed with dashed lines and its pertinent phase fields are labeled with parentheses. Melts heated to temperatures indicated by the dashed line (a) obey crystallization path in accordance with the equilibrium phase diagram. Melts cooled down from temperatures above the line (a) will follow metastable path of solidification.

## METASTABILITY

### Formation of Two Liquids

Observation of liquids of YAG composition during crystal growth revealed that they are always opaque, in contrast to  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$  melts, which are transparent. Formation of two immiscible liquids appeared to be a possible explanation of the opacity. Since the metastable eutectic has been determined between  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$ , it was inferred that, after melting, YAG forms two immiscible liquids,  $\text{Al}_2\text{O}_3$  and  $\text{YAlO}_3$ . To prove this hypothesis the following experiment was conducted.

Table 4. TEMPERATURES OF SOLIDUS AND LIQUIDUS MEASURED BY ODTA

Composition		Mixture Sintered 48 Hr at 1100 C		Mixture Melted and Heated to 2000 C		Perovskite to Garnet Transformation Deg C
Mol. % Y <sub>2</sub> O <sub>3</sub>	Mol. % Al <sub>2</sub> O <sub>3</sub>	Solidus Deg C	Liquidus Deg C	Solidus Deg C	Liquidus Deg C	
10.0	90.0	1823	1942	1700	1936	1418
18.5	81.5	-	1826	1700	1819	1419
23.0	67.0	1822	1960	-	1701	1416
27.5	72.5	1820	1890	1698	1761	1418
32.5	67.5	1822	1914	1707	1820	1418
37.5	62.5	-	1940	1702	1855	N.M.
40.0	60.0	1909	1933	1700	1880	1419
43.0	57.0	1909	1930	1700	1825	N.M.
45.0	55.0	-	1909	1700	1890	1418
47.5	52.5	1909	1916	1700	1907	N.M.
50.0	50.0	1916	1934	1914	1935	-

N.M. = Not Measured

In the absence of motion, immiscible liquids with different densities will tend to stratify. In practice, however, convection currents exist which agitate the liquid. To avoid thermal agitation of the melt, the HEM technique, which minimizes convection currents because of stabilizing temperature gradients, was selected to achieve the stratification of the immiscible liquids. For this purpose, crushed YAG single crystals were melted in a cylindrical crucible in a crystal growth furnace and held for 4 hours at 1990 C. After holding the melt unstirred and in thermal stable conditions for this length of time it was assumed, due to the density difference that the  $\text{YAlO}_3$  melt would be situated in the lower part of the crucible where the supercooling is highest and where nucleation should occur first. To encourage localized nucleation, a heat sink of small diameter was located at the center of the crucible bottom. After routine solidification used for growing single crystals by the HEM technique,<sup>10</sup> the solid material was examined by X-ray Laue method and optical microscopy. The examination revealed that the entire bottom of the crucible was covered with a single crystal of  $\text{YAlO}_3$  (see Figure 7). Since the  $\text{YAlO}_3$  crystal grew from the melt of YAG composition, the constitutional supercooling instituted dendritic growth. The  $\text{YAlO}_3$  dendrites shown in Figure 8 grew in the [001] direction. The nonreacted  $\text{Al}_2\text{O}_3$  was found as a eutectic dispersion adhering to the lower parts of the dendrites. In spite of positive results, this experiment does constitute only indirect evidence to confirm the existence of two immiscible liquids. Microscopic examination of microstructures of metastably solidified mixtures of  $\text{Al}_2\text{O}_3$  and  $\text{Y}_2\text{O}_3$  ranging from 25 to 50 mol. %  $\text{Y}_2\text{O}_3$  revealed that  $\text{YAlO}_3$  is always the pro-eutectic phase; hence,  $\text{YAlO}_3$  will nucleate first whether the liquids are separated

10. CASLVASKY, J. L., and VIECHNICKI, D. J. *Melt Growth of  $\text{Nd:Y}_2\text{Al}_3\text{O}_{12}$  (Nd:YAG) Using the Heat Exchanger Method (HEM)*. J. Crystal Growth, v. 46, 1979, p. 601-606.



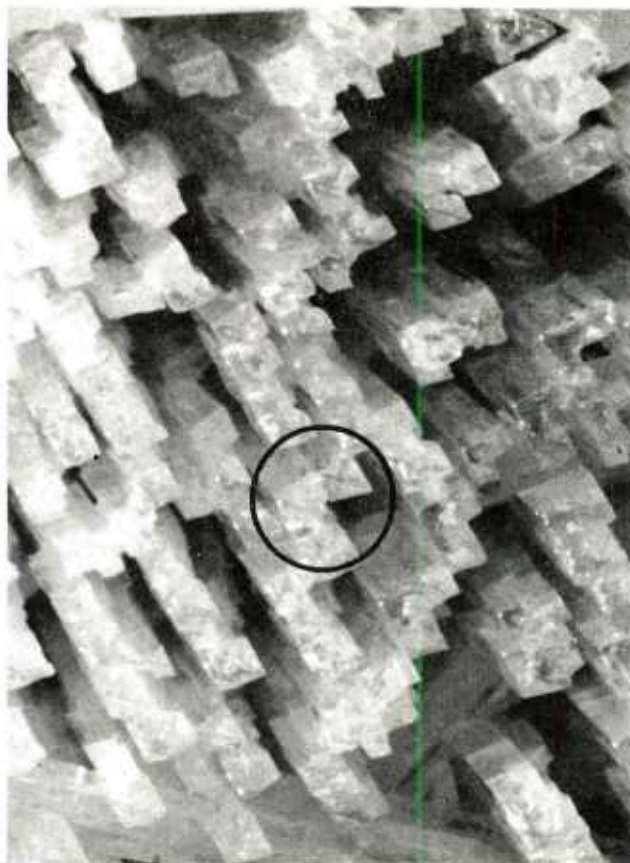


Figure 7. Perovskite twin on the bottom of  $\text{YAlO}_3$  single crystal grown from the melt of  $\text{Y}_3\text{Al}_5\text{O}_{12}$  composition.

Figure 8. Dendrites finalizing the growth of the perovskite crystal shown in Figure 7. Note the perovskite twin on tips of dendrites in circled area.

or not. Furthermore, study of liquids of YAG composition by ODTA up to 2050 C did not reveal and  $\Delta H$  change in the melt; therefore the opacity of the YAG melt is the only evidence for existence of two immiscible liquids in the  $\text{Al}_2\text{O}_3 - \text{Y}_2\text{O}_3$  binary system.

### Change of Aluminum Coordination

The fact that  $\text{YAlO}_3$  melts incongruently limits its existence to temperatures below the peritectic temperature. From this point of view it is unlikely to expect the formation of two liquids, one of which has the composition of an incongruently melting compound, i.e.,  $\text{YAlO}_3$ . Therefore, a more reasonable explanation of the preferential formation of nonequilibrium  $\text{YAlO}_3$  over the YAG structure seems to lie in the fact that the aluminum has to decrease its coordination in order to form the garnet structure.

Aluminum-oxygen octahedra are the most important structural elements in solid and molten structures of aluminum oxide. It is not unreasonable to expect that the solid structure most similar to the short range order of the liquid will

be energetically favored and likely will form whether or not it is stable under the existing equilibrium conditions. As seen from Figure 6,  $\text{YA10}_3$  (in the composition range 10.0 mol. % to 47.5 mol. %  $\text{Y}_2\text{O}_3$ ) transforms to YAG in solid state at 1418 C. This transformation is accompanied by the volume change evidenced by the crucible expansion (see Figure 9), and has endothermic character which is observed by ODTA (see Figure 10) both those effects confirms that the YAG structure has a higher energy of formation than the perovskite structure. The higher free energy of the YAG structure results from the necessity to force aluminum into a fourfold coordination site to form YAG.

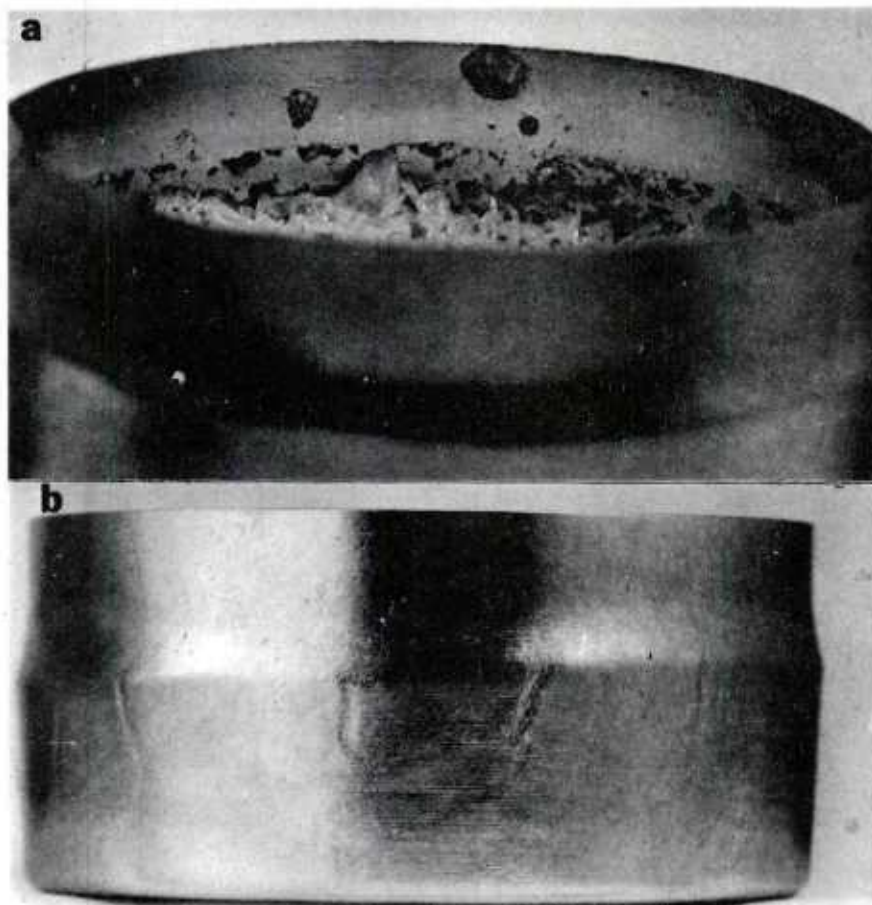


Figure 9. Photographs of the molybdenum crucible (25-mm in diameter). (a) Displays relation between height of the solid with respect to deformation of crucible. (b) Wall expanded due to transformation of metastably frozen mixture of 67.5 mol. %  $\text{Al}_2\text{O}_3$  and 32.5 mol. %  $\text{Y}_2\text{O}_3$ .

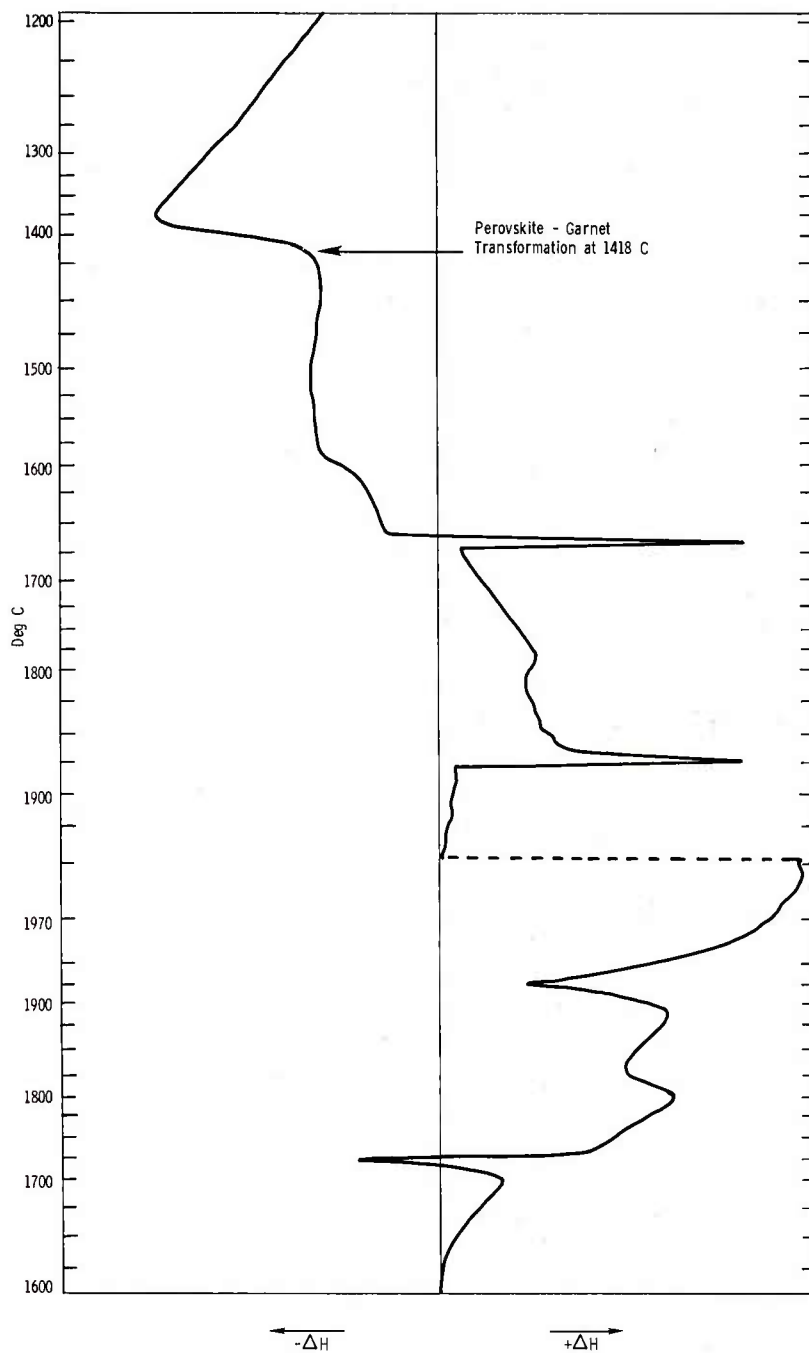


Figure 10. ODTA curve of melting and freezing of 90 mol. %  $\text{Al}_2\text{O}_3$  and 10 mol. %  $\text{Y}_2\text{O}_3$  reacted by melting.

## CONCLUSIONS

YAG melts congruently and is stable to its melting point at  $1940 \pm 7$  C.  $\text{YAlO}_3$  (perovskite) melts incongruently with a peritectic at  $1916 \pm 7$  C and a liquidus at  $1934 \pm 7$  C. A metastable phase diagram was defined with a metastable

eutectic at 23 mol. %  $\text{Y}_2\text{O}_3$  - 77 mol. %  $\text{Al}_2\text{O}_3$  and  $1702 \pm 7$  C.  $\text{YAlO}_3$  formed during metastable solidification transforms to YAG in the presence of  $\text{Al}_2\text{O}_3$  at  $1418 \pm 7$  C.

When melt temperatures do not exceed 1940 C, the melts of  $\text{Y}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$ , ranging in composition from 10 to 45 mol. % of  $\text{Y}_2\text{O}_3$ , retain aluminum in fourfold coordination; therefore, they obey the crystallization path of the equilibrium phase diagram. However, at approximately 2000 C a structural change takes place in the liquid; consequently the melts cooled down from temperatures above 2000 C follow the crystallization path of the metastable phase diagram. The metastability is due to the fact that aluminum prefers the six-coordination in the melt, which also explains the difficulty of growing YAG single crystals from melt, since the growth rate is predominantly controlled by the rate of a decrease in the aluminum coordination.

Furthermore, recent studies of  $\text{Al}_2\text{O}_3$ - $\text{Nd}_2\text{O}_3$ - $\text{Y}_2\text{O}_3$  ternary phase relations by ODTA indicate that neodymia destabilizes the fourfold coordination of aluminum, which increases the difficulty in growing Nd:YAG single crystals of laser quality.

#### ACKNOWLEDGMENTS

The authors are indebted to Dr. R. Roy and Dr. W. B. White for their critical reading of the manuscript and constructive suggestions, and to W. Earle for his valuable assistance with the experimental aspects of this work.

Portions of this work were made possible by the support of the U.S. Army Missile Command, through MM&T project 3783126(2597) "Processing of Laser Optical Ceramics."



## DISTRIBUTION LIST

No. of Copies	To	No. of Copies	To
	Office of the Under Secretary of Defense for Research and Engineering, The Pentagon, Washington, D.C. 20301		Commander, U.S. Army Mobility Equipment Research and Development Command, Fort Belvoir, Virginia 22060
1	ATTN: Mr. J. Persh	1	ATTN: DRDME-EM, Mr. W. McGovern
1	Or. G. Gamota	1	DRDME-V, Mr. E. York
12	Commander, Defense Documentation Center, Cameron Station, Building S, 5010 Duke Street, Alexandria, Virginia 22314	1	DRDME-X, Mr. H. J. Peters
1	National Technical Information Service, 5285 Port Royal Road, Springfield, Virginia 22161		Director, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, Maryland 21005
	Director, Defense Advanced Research Projects Agency, 1400 Wilson Boulevard, Arlington, Virginia 22209	1	ATTN: DRDAR-TSB-S (STINFO)
1	ATTN: Or. A. Bement	1	Commander, Rock Island Arsenal, Rock Island, Illinois 61299
1	Or. Van Reuth	1	ATTN: SARRI-EN
1	MAJ Harry Winsor		Commander, U.S. Army Test and Evaluation Command, Aberdeen Proving Ground, Maryland 21005
	Battelle Columbus Laboratories, Metals and Ceramics Information Center, 505 King Avenue, Columbus, Ohio 43201	1	ATTN: DRSTE-ME
1	ATTN: Mr. Winston Duckworth		Commander, U.S. Army Foreign Science and Technology Center, 220 7th Street, N.E., Charlottesville, Virginia 22901
1	Or. D. Niesz	1	ATTN: Military Tech, Mr. W. Marley
	Deputy Chief of Staff, Research, Development, and Acquisition, Headquarters, Department of the Army, Washington, D.C. 20310		Chief, Benet Weapons Laboratory, LWSL, USA ARRADCOM, Watervliet, New York 12189
1	ATTN: DAMA-ARZ	1	ATTN: DRDAR-LCB-TL
1	DAMA-CSS, Dr. J. Bryant		Commander, Watervliet Arsenal, Watervliet, New York 12189
1	DAMA-PPP, Mr. R. Vawter	1	ATTN: Dr. T. Davidson
	Commander, U.S. Army Research and Development Office, Chief Research and Development, Washington, D.C. 20315		Director, Eustis Directorate, U.S. Army Mobility Research and Development Laboratory, Fort Eustis, Virginia 23604
1	ATTN: Physical and Engineering Sciences Division	1	ATTN: Mr. J. Robinson, SAVDL-E-MOS (AVRADCOM)
	Commander, Army Research Office, P.O. Box 12211, Research Triangle Park, North Carolina 27709	1	Mr. C. Walker
1	ATTN: Information Processing Office		Commander, U.S. Army Engineer Waterways Experiment Station, Vicksburg, Mississippi 39180
1	Dr. G. Mayer	1	ATTN: Research Center Library
1	Or. J. Hurt		Project Manager, Munitions Production Base, Modernization and Expansion, Dover, New Jersey 07801
	Commander, U.S. Army Materiel Development and Readiness Command, 5001 Eisenhower Avenue, Alexandria, Virginia 22333	1	ATTN: ORCPM-PBM-P
1	ATTN: ORCDMO-ST		Technical Director, Human Engineering Laboratories, Aberdeen Proving Ground, Maryland 21005
1	ORCLOC, Mr. R. Zentner	1	ATTN: Technical Reports Office
	Commander, U.S. Army Electronics Research and Development Command, Fort Monmouth, New Jersey 07703		Chief of Naval Research, Arlington, Virginia 22217
1	ATTN: DELSD-L	1	ATTN: Code 471
1	T. Aucoin	1	Or. A. Oiness
	Commander, U.S. Army Materiel Systems Analysis Activity, Aberdeen Proving Ground, Maryland 21005	1	Or. R. Pohanka
1	ATTN: DRXSY-MP, H. Cohen		Naval Research Laboratory, Washington, D.C. 20375
	Commander, U.S. Army Night Vision Electro-Optics Laboratory, Fort Belvoir, Virginia 22060	1	ATTN: Or. J. M. Krafft - Code B430
1	ATTN: OELNV-S, Mr. P. Travesky	1	Mr. R. Rice
1	OELNV-L-O, Or. R. Buser		Headquarters, Naval Air Systems Command, Washington, D.C. 20360
	Commander, Harry Diamond Laboratories, 2800 Powder Mill Road, Adelphi, Maryland 20783	1	ATTN: Code S203
1	ATTN: Mr. A. Benderly	1	Code MAT-D42M
1	Technical Information Office	1	Mr. C. F. Bersch
1	OELHO-RAE	1	Mr. I. Machlin
	Commander, U.S. Army Missile Command, Redstone Arsenal, Alabama 35809		Headquarters, Naval Sea Systems Command, 1941 Jefferson Davis Highway, Arlington, Virginia 22376
1	ATTN: Mr. P. Ormsby	1	ATTN: Code 03S
1	Technical Library		Headquarters, Naval Electronics Systems Command, Washington, D.C. 20360
1	ORSMI-TB, Redstone Scientific Information Center	1	ATTN: Code S04
1	ORSMI-EAT, Mr. Ray Farrison		Commander, Naval Ordnance Station, Louisville, Kentucky 40214
1	DRSMI-EAT, Mr. Bobby Park	1	ATTN: Code B5
	Commander, U.S. Army Aviation Research and Development Command, P.O. Box 209, St. Louis, Missouri 63166		Commander, Naval Material Industrial Resources Office, Building S37-2, Philadelphia Naval Base, Philadelphia, Pennsylvania 19112
1	ATTN: DRDAV-EXT	1	ATTN: Technical Director
1	DRDAV-QE		Commander, Naval Weapons Center, China Lake, California 93555
1	Technical Library	1	ATTN: Mr. F. Markarian
	Commander, U.S. Army Natick Research and Development Command, Natick, Massachusetts 01760	1	Mr. E. Teppo
1	ATTN: Technical Library	1	Mr. M. Ritchie
	Commander, U.S. Army Satellite Communications Agency, Fort Monmouth, New Jersey 07703		Commander, U.S. Air Force of Scientific Research, Building 410, Bolling Air Force Base, Washington, D.C. 20332
1	ATTN: Technical Document Center	1	ATTN: MAJ W. Simmons
	Commander, U.S. Army Tank-Automotive Research and Development Command, Warren, Michigan 48090		Commander, U.S. Air Force Materials Laboratory, Wright-Patterson Air Force Base, Ohio 45433
1	ATTN: Dr. W. Bryzik	1	ATTN: Dr. N. Tallan
1	Mr. E. Hamperian	1	Dr. H. Graham
1	D. Rose	1	Dr. R. Ruh
1	DRDTA-RKA, Dr. J. Chevalier	1	Mr. K. S. Mazdhyasni
1	OROTA-UL, Technical Library	1	Aero Propulsion Labs, Mr. R. Marsh
1	DRDTA-R		Commander, Air Force Weapons Laboratory, Kirtland Air Force Base, Albuquerque, New Mexico 87115
	Commander, U.S. Army Armament Research and Development Command, Dover, New Jersey 07801	1	ATTN: Dr. R. Rudder
1	ATTN: Mr. J. Lannon		Commander, Air Force Armament Center, Eglin Air Force Base, Florida 32542
1	Or. G. Vezzoli	1	ATTN: Technical Library
1	Mr. A. Graf		National Aeronautics and Space Administration, Washington, D.C. 20546
1	Mr. Harry E. Peibly, Jr., PLASTEC, Director	1	ATTN: Mr. G. C. Oetusch - Code RW
1	Technical Library	1	Mr. J. Gangler
	Commander, U.S. Army Armament Materiel Readiness Command, Rock Island, Illinois 61299	1	AFSS-AO, Office of Scientific and Technical Information
1	ATTN: Technical Library		
	Commander, Aberdeen Proving Ground, Maryland 21005		
1	ATTN: DRDAR-CLB-PS, Mr. J. Vervier		

No. of Copies	To
	National Aeronautics and Space Administration, Langley Research Center, Hampton, Virginia 23665
1	ATTN: Mr. J. Buckley, Mail Stop 387
	Commander, White Sands Missile Range, Electronic Warfare Laboratory, OMEW, ERAOCOM, White Sands, New Mexico 88002
1	ATTN: Mr. Thomas Reader, DRSEL-WLM-ME
	Department of Energy, Division of Transportation, 20 Massachusetts Avenue, N.W., Washington, D.C. 20545
1	ATTN: Mr. George Thur (TEC)
1	Mr. Robert Schulz (TEC)
1	Mr. John Neal (CLNRT)
1	Mr. Steve Wander (Fossil Fuels)
	National Bureau of Standards, Washington, D.C. 20234
1	ATTN: Or. S. Wiederhorn
1	Or. J. B. Wachtmann
	National Research Council, National Materials Advisory Board, 2101 Constitution Avenue, Washington, D.C. 20418
1	ATTN: Or. W. Prindle
1	O. Groves
1	R. M. Spriggs
	National Science Foundation, Washington, D.C. 20550
1	ATTN: B. A. Wilcox
	Admiralty Materials Technology Establishment, Polle, Dorset BH16 6JU, United Kingdom
1	ATTN: Or. O. Godfrey
1	Or. M. Lindley
	AVCO Corporation, Applied Technology Division, Lowell Industrial Park, Lowell, Massachusetts 01887
1	ATTN: Dr. T. Vasilos
	California Institute of Technology JPL 157-361, Pasadena, California 91103
1	ATTN: Dr. P. J. Shlichta, Director of Material Science
	Case Western Reserve University, Department of Metallurgy, Cleveland, Ohio 44106
1	ATTN: Prof. A. H. Heuer
	Crystal Systems, Inc., P.O. Box 1057, Salem, Massachusetts 01970
1	ATTN: Mr. F. Schmid
	Defence Research Establishment Pacific, FMO, Victoria, B.C., VDS 1B0, Canada
1	ATTN: R. D. Barer
	European Research Office, 223 Old Marylebone Road, London, NW1 - 5th, England
1	ATTN: Dr. R. Quattrone
1	LT COL James Kennedy
	Ford Motor Company, Turbine Research Department, 20000 Rotunda Drive, Dearborn, Michigan 48121
1	ATTN: Mr. A. F. McLean
1	Mr. E. A. Fisher
	General Electric Company, Research and Development Center, Box 8, Schenectady, New York 12345
1	ATTN: Dr. R. J. Charles
1	Dr. C. D. Greskovich
1	Dr. S. Prochazka
	General Motors Corporation, AC Spark Plug Division, Flint, Michigan 48556
1	ATTN: Dr. M. Berg
	Georgia Institute of Technology, EES, Atlanta, Georgia 30332
1	ATTN: Mr. J. D. Walton
	GTE Laboratories, Waltham Research Center, 40 Sylvan Road, Waltham, Massachusetts 02154
1	ATTN: Dr. C. Quackenbush
1	Dr. W. H. Rhodes
	Hughes Aircraft Company, Industrial Products Division, 6155 El Camino Real, Carlsbad, California 92008
1	ATTN: Dr. Edward L. Kern, Manager, Solid State Products
	Hughes Research Laboratories, A Division of Hughes Aircraft Company, 3011 Malibu Canyon Road, Malibu, California 90265
1	ATTN: Dr. Gerald S. Picus, Manager, Chemical Physical Dept.
1	Dr. R. C. Pastor
1	Dr. Anthony L. Gentile
1	Dr. Sanat R. Sashital
1	Dr. Larry G. Shazer
1	Mr. Don DeVore
	IIT Research Institute, 10 West 35th Street, Chicago, Illinois 60616
1	ATTN: Mr. S. Bortz, Director, Ceramics Research
	Institute für Werkstoff-Forschung, DFVLR, 505 Porz-Wahn, Linder Höhe, Germany
1	ATTN: Dr. W. Bunk
1	Dr. H. Knoch
	International Harvester, Solar Division, 2200 Pacific Highway, P.O. Box 80966, San Diego, California 92138
1	ATTN: Dr. A. Metcalfe
1	Ms. M. E. Gulden
	Lambda/Airtron Division, Litton Industries, 200 E. Hanover Ave., Morris Plains, New Jersey 07950
1	ATTN: Dr. Roger Belt

No. of Copies	To
	Martin Marietta Laboratories, 1450 South Rolling Road, Baltimore, Maryland 21227
1	ATTN: Dr. J. Venables
	Massachusetts Institute of Technology, Department of Metallurgy and Materials Science, Cambridge, Massachusetts 02139
1	ATTN: Prof. R. L. Coble
1	Prof. H. K. Bowen
1	Prof. W. O. Kingery
	Materials Research Laboratories, P.O. Box 50, Ascot Vale, VIC 3032, Australia
1	ATTN: Or. C. W. Weaver
	Midwest Research Institute, 425 Volker Boulevard, Kansas City, Missouri 64110
1	ATTN: Mr. Gordon W. Gross, Head, Physics Station
	Monsanto Electronic Products Division, P.O. Box 8, St. Peters, Missouri 63376
1	ATTN: Or. Milan Kozak
	Norton Company, Worcester, Massachusetts 01606
1	ATTN: Dr. N. Ault
1	Dr. M. L. Torti
	Pennsylvania State University, Materials Research Laboratory, Materials Science Department, University Park, Pennsylvania 16802
1	ATTN: Prof. R. Roy
1	Prof. R. E. Newnham
1	Prof. R. E. Tressler
1	Prof. R. Bradt
1	Prof. V. S. Stubican
	PSC, Box 1044, APO San Francisco 96328
1	ATTN: MAJ A. Anthony Borges
	RIAS, Division of the Martin Company, Baltimore, Maryland
1	ATTN: Dr. A. R. C. Westwood
	Rockwell International, Electronics Research Division, 3370 Miraloma Avenue, Anaheim, California 92803
1	ATTN: Mr. S. Austerman
	Rockwell International Science Center, 1049 Camino Dos Rios, P.O. Box 1085, Thousand Oaks, California 91360
1	ATTN: Dr. Ratnakar R. Neurgaonkar
	Royal Aircraft Establishment, Materials Department, R 17B Building, Farnborough, Hants, England
1	ATTN: Dr. N. Corney
	Shane Associates, Inc., 7821 Carrleigh Parkway, Springfield, Virginia 22152
1	ATTN: Or. Robert S. Shane, Consultant
	Stanford Research International, 333 Ravenswood Avenue, Menlo Park, California 94025
1	ATTN: Dr. P. Jorgensen
1	Dr. D. Rowcliffe
	State University of New York at Stony Brook, Department of Materials Science, Long Island, New York 11790
1	ATTN: Prof. Franklin F. Y. Wang
	Union Carbide Corp., Crystal Products Division, San Diego, California 92123
1	ATTN: Dr. W. Brandle
	United Technologies Research Center, East Hartford, Connecticut 06108
1	ATTN: Dr. J. Brennan
1	Dr. F. Galasso
	University of California, Lawrence Livermore Laboratory, P.O. Box BDB, Livermore, California 94550
1	ATTN: O. M. J. Weber
1	Dr. C. F. Cline
	University of Florida, Department of Materials Science and Engineering, Gainesville, Florida 32601
1	ATTN: Dr. L. Hench
	University of Newcastle Upon Tyne, Department of Metallurgy and Engineering Materials, Newcastle Upon Tyne, NE1 7 RU, England
1	ATTN: Prof. K. H. Jack
	University of Washington, Ceramic Engineering Division, FB-10, Seattle, Washington 98195
1	ATTN: Prof. James I. Mueller
	Varian Solid State West, 611 Hansen Way, Palo Alto, California 94303
1	ATTN: Dr. Miro Vichr
	Westinghouse Electric Corporation, Research Laboratories, Pittsburgh, Pennsylvania 15235
1	ATTN: Dr. R. J. Bratton
1	Dr. B. Rossing
	Director, Army Materials and Mechanics Research Center, Watertown, Massachusetts 02172
2	ATTN: DRXMR-PL
1	DRXMR-WO
2	Authors

Army Materials and Mechanics Research Center,  
Watertown, Massachusetts 02172  
STUDY OF THE MELTING BEHAVIOR OF  
YAG SINGLE CRYSTAL BY

OPTICAL DIFFERENTIAL THERMAL ANALYSIS -

Jaroslav L. Caslavsky and Dennis J. Viechnicki

Technical Report AMMRC TR 79-56, November 1979, 17 pp -  
illus-tables, O/A Project 1T162105AH84,  
AMCMS Code 612105

AO UNCLASSIFIED  
UNLIMITED DISTRIBUTION

Key Words

Yttrium aluminum garnet (YAG)  
Phase equilibria  
Laser materials

The melting point of yttrium aluminum garnet (YAG), reinvestigated by optical differential thermal analysis (ODTA), was found to be  $1940 \pm 7$  C. Above this temperature YAG liquids are opaque, suggesting the presence of two immiscible liquids. In the composition range 10.0 to 47.5 mol. %  $Y_2O_3$ , crystallization of the equilibrium phases can only occur in the presence of YAG nuclei; otherwise solidification of  $YAlO_3$  and  $Al_2O_3$  will take place. A metastable phase diagram has been defined with a metastable eutectic at 23 mol. %  $Y_2O_3$  - 77 mol. %  $Al_2O_3$  and  $1702 \pm 7$  C.  $YAlO_3$  (perovskite) was found to melt incongruently with a peritectic temperature of  $1916 \pm 7$  C and a liquidus temperature of  $1934 \pm 7$  C.  $YAlO_3$  formed during metastable solidification transforms to YAG in the presence of  $Al_2O_3$  at  $1418 \pm 7$  C. It is suggested that the metastability arises from the difficulty of the aluminum to attain fourfold coordination in the YAG structure.

Army Materials and Mechanics Research Center,  
Watertown, Massachusetts 02172  
STUDY OF THE MELTING BEHAVIOR OF  
YAG SINGLE CRYSTAL BY

OPTICAL DIFFERENTIAL THERMAL ANALYSIS -

Jaroslav L. Caslavsky and Dennis J. Viechnicki

Technical Report AMMRC TR 79-56, November 1979, 17 pp -  
illus-tables, O/A Project 1T162105AH84,  
AMCMS Code 612105

AO

UNCLASSIFIED  
UNLIMITED DISTRIBUTION

Key Words

Yttrium aluminum garnet (YAG)  
Phase equilibria  
Laser materials

The melting point of yttrium aluminum garnet (YAG), reinvestigated by optical differential thermal analysis (ODTA), was found to be  $1940 \pm 7$  C. Above this temperature YAG liquids are opaque, suggesting the presence of two immiscible liquids. In the composition range 10.0 to 47.5 mol. %  $Y_2O_3$ , crystallization of the equilibrium phases can only occur in the presence of YAG nuclei; otherwise solidification of  $YAlO_3$  and  $Al_2O_3$  will take place. A metastable phase diagram has been defined with a metastable eutectic at 23 mol. %  $Y_2O_3$  - 77 mol. %  $Al_2O_3$  and  $1702 \pm 7$  C.  $YAlO_3$  (perovskite) was found to melt incongruently with a peritectic temperature of  $1916 \pm 7$  C and a liquidus temperature of  $1934 \pm 7$  C.  $YAlO_3$  formed during metastable solidification transforms to YAG in the presence of  $Al_2O_3$  at  $1418 \pm 7$  C. It is suggested that the metastability arises from the difficulty of the aluminum to attain fourfold coordination in the YAG structure.